

RECORDING/REPRODUCING APPARATUS AND REPRODUCING APPARATUS

CROSS REFERENCE TO RELATED APPLICATION

This is a continuation of U.S. application Serial No.
09/090,339, filed June 4, 1998, the subject matter of which is
incorporated by reference herein.

BACKGROUND OF THE INVENTION

The present invention relates to a system construction and so on for realizing a long play recording/reproducing system such as a recording/
5 reproducing apparatus and a reproducing apparatus.

Conventionally, for example, in VHS standard magnetic recording/reproducing apparatuses or video tape recorders (VTR), there has been realized a long play recording mode of a triple mode in which a magnetic tape
10 runs at a speed equal to 1/3 of a standard tape running speed. These techniques have been disclosed by, for example, JP-A-59-124004 and so on. Also, various data input means using a control signal on a magnetic tape include techniques disclosed by, for example,
15 JP-A-62-33388 and so on. Further, high-speed fast feed/rewind techniques have been disclosed by, for example, JP-A-1-217752.

SUMMARY OF THE INVENTION

There are very strong demands for long play
20 recording and longer play recording apparatuses are desired. However, it is necessary to realize a reasonable system while maintaining the compatibility with the conventional standard play recording mode. Therefore, an object of the present invention is to

realize a long play recording mode while following the conventional system while solving problems inclusive of the construction of rotary audio and video heads, a control method for automatic tracking and a control
5 technique at the time of high-speed fast feed/rewind which newly arise in realizing the long play mode.

To attain the above object, the present invention provides a recording/reproducing apparatus of a helical scan system for recording a video signal and an
10 audio signal in a superimposed manner on a magnetic tape by use of magnetic head means mounted on a rotary body or reproducing such recorded signals by use of the magnetic head means, characterized in that the magnetic head means includes first and second video heads for recording or
15 reproducing a video signal at the time of standard play mode in which the running speed of the magnetic tape is a standard speed, third and fourth video heads for recording or reproducing a video signal at the time of N-ple play mode in which the tape running speed is
20 approximately $1/N$ of the standard speed wherein N is an integer not smaller than 4, and first and second audio heads for recording or reproducing an audio signal, the video and audio heads being provided on the outer periphery of the rotary body, that the first and second
25 video heads, the third and fourth video heads, and the first and second audio heads are respectively provided in pairs so that the heads in each pair are arranged at positions which are substantially symmetrical with

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respect to a rotation axis of the rotary body, the gap
planes of the paired heads being tilted relative to a
plane perpendicular to a head rotation direction by equal
angles in different directions, and the tilt angles of
5 the first and second audio heads being different from the
tilt angles of the first and second video heads and the
third and fourth video heads, and that the recording is
performed so that the first and second video heads or the
third and fourth video heads record a video signal in a
10 superimposed manner on a track having an audio signal
recorded on the magnetic tape by the first and second
audio heads.

Also, it is characterized in that the first and
fourth video heads having their gap planes with different
15 titling directions are arranged in proximity to each
other to form one pair while the second and third video
heads having their gap planes with different titling
directions are arranged in proximity to each other to
form one pair, these pairs being respectively arranged
20 rearward of the arranging positions of said first and
second audio heads by approximately 120 degree along the
head rotation direction so that the heights of the
centers of the head widths of these video heads measured
from a reference surface of the body substantially
25 coincide with each other.

In this case, it is preferable that the head
width of each of the first and second audio heads is not
larger than three times as large as a track pitch formed

There can be provided automatic tracking means for performing a tracking control by use of a signal reproduced by the first and second audio heads when a

The head width of each of the third and fourth video heads is approximately two times as large as a track pitch formed on the magnetic tape at the time of N-ple play mode.

Also, it is preferable that the heights of arrangement of the third and fourth video heads and the first and second audio heads relative to a reference surface of the rotary body are set to positions with which at the time of N-ple play mode, the third and fourth video heads scan the magnetic tape in a manner delayed from the first and second audio heads by four or more tracks. Further, it is preferable that at the time of completion of recording, the stop of supply of an audio recording signal to the first and second audio heads is followed by the supply of a video recording signal to the third and fourth video heads with a time prolonged corresponding to the delay of scan of the magnetic tape by the third and fourth video heads from that by the first and second audio heads.

25 Further, the recording/reproducing apparatus of
the present invention is characterized in that first and
second video heads for recording or reproducing a video
signal at the time of standard play mode in which the

running speed of the magnetic tape is a standard speed, third and fourth video heads for recording or reproducing a video signal at the time of triple play mode in which the tape running speed is approximately $1/3$ of the

- 5 standard speed, and first and second audio heads for recording or reproducing an audio signal are provided as the magnetic head means on the outer periphery of the rotary body, and that at the time of N-ple play mode in which the tape running speed is approximately $1/N$ of the
- 10 standard speed wherein N is an integer not smaller than 4, the recording is performed so that the third and fourth video heads record a video signal in a super-imposed manner on a track having an audio signal recorded on the magnetic tape by the first and second audio heads.
- 15 In this case, the head width of each of the third and fourth video heads recording or reproducing a video signal at the time of triple play mode and at the time of N-ple play mode is substantially equal to a track pitch at the time of triple play mode.

- 20 Further, the recording/reproducing apparatus of the present invention is characterized by comprising first and second video heads for alternately forming recording tracks on a recording medium, delay means for delaying at least one of video recording signals supplied
- 25 to the first and second video heads, and delay control means for controlling a delay time of the delay means substantially for each recording track, the delay control means making a control so that horizontal synchronizing

signals recorded on the recording medium are arranged between adjacent recording tracks.

Further, the recording/reproducing apparatus of the present invention is characterized by comprising means for making the switching between a first recording/reproducing mode in which the recording/reproducing is performed with the recording medium being run at a first running speed and with the rotary body being rotated at a first rotating speed, a second recording/reproducing mode in which the recording/reproducing is performed with the recording medium being run at a second running speed and with the rotary body being rotated at said first rotating speed, and a third recording/reproducing mode in which the recording/reproducing is performed with the recording medium being run at a third running speed and with the rotary body being rotated at a second rotating speed. In this case, it is preferable that the second running speed is $1/N$ of the first running speed wherein N is an integer not smaller than 2, the third running speed is $1/M$ of the second running speed wherein M is an integer not smaller than 2, and the second rotating speed is $1/M$ of the first rotating speed wherein M is an integer not smaller than 2.

Further, the recording/reproducing apparatus of
25 the present invention is characterized by comprising
means for making the switching between a first recording
mode in which a video signal corresponding to one field
is recorded on one recording track and a second recording

mode in which a video signal corresponding to M fields is recorded on one recording track wherein M is an integer not smaller than 2.

Also, the present invention provides a

- 5 reproducing apparatus of a helical scan system for
reproducing a video signal and an audio signal by use of
magnetic head means mounted on a rotary body, the video
signal and the audio signal being recorded in a super-
imposed manner on a magnetic tape, characterized in that
10 the magnetic head means includes first, second, third and
fourth video heads and first and second audio heads, and
that there is provided means for making the switching
between a standard play reproducing mode for causing the
first and second video heads and the first and second
15 audio heads to reproduce a video signal and an audio
signal recorded in a standard play mode in which the
running speed of the magnetic tape is a standard speed, a
triple play reproducing mode for causing the third and
fourth video heads and the first and second audio heads
20 to reproduce a video signal and an audio signal recorded
in a triple play mode in which the tape running speed is
approximately $1/3$ of the standard speed, and a N-ple play
reproducing mode for causing the third and fourth video
heads and the first and second audio heads to reproduce a
25 video signal and an audio signal recorded in an N-ple
play mode in which the tape running speed is approxi-
mately $1/N$ of the standard speed wherein N is an integer
not smaller than 4. It is further characterized in that

there is included a double play reproducing mode for causing the first and second video heads and the first and second audio heads to reproduce a video signal and an audio signal recorded in a double play mode in which the
5 tape running speed is approximately $1/2$ of the standard speed.

Also, the reproducing apparatus of the present invention is characterized by comprising speed setting means by which a tape running speed when a magnetic tape
10 subjected to recording in an N-ple play mode with a tape running speed equal to approximately $1/N$ (N: an integer not smaller than 4) of a standard speed is subjected to high-speed fast feed or rewind is set to be lower than a tape running speed when a magnetic tape subjected to
15 recording in a standard play mode with a tape running speed equal to the standard speed is subjected to high-speed fast feed or rewind. In this case, it is desirable that the speed is set so that it falls within a speed range in which a control signal reproduced from the
20 magnetic tape is detectable, preferably, for example, a speed range in which the duty of a control signal reproduced from the magnetic tape can be discriminated.

In the recording/reproducing apparatus and the reproducing apparatus mentioned above, it is preferable
25 that the value of N is 5 or 6. Further, thereby making it possible to set the value of N by arbitrarily selecting an integer not smaller than 4 from among a plurality of values.

Also, it is preferable that the recording/
reproducing apparatus or the reproducing apparatus is a
video tape recorder based on a VHS system. These
apparatuses is provided with medium detecting means for
5 detecting the type of the recording medium, whereby the
running speed of the recording medium and the rotating
speed of the rotary body can be set or selected in
accordance with the result of having detected the kind of
the medium.

10 BRIEF DESCRIPTION OF THE DRAWINGS

These and other features, objects and
advantages of the present invention will become more
apparent from the following description when taken in
conjunction with the accompanying drawings:

15 Fig. 1 is a diagram showing an embodiment of
the head construction of a magnetic recording/reproducing
apparatus according to the present invention;

Fig. 2 is a diagram showing the arrangement of
heads shown in Fig. 1;

20 Fig. 3 is a pattern diagram showing a relative
positional relationship between a tape and heads at the
time of recording in a standard play mode;

Fig. 4 is a pattern diagram showing a relative
positional relationship between a tape and heads in a
25 sextuple play mode to which the present invention is
applied;

Fig. 5 is a diagram showing the relative

positional relationship representing the recording stop timings of a video head and an audio head at the time of stop of recording in the sextuple play mode to which the present invention is applied;

5 Fig. 6 is a circuit block diagram for realizing the relationship shown in Fig. 5;

 Fig. 7 is a diagram showing a relative positional relationship representing a relationship in tracking phase between a tape and heads at the time of reproduction in the sextuple play mode to which the
10 present invention is applied;

 Fig. 8 is a diagram showing a relative positional relationship between a tape and heads at the time of search reproduction in the standard play mode to
15 which the present invention is applied;

 Fig. 9 is a circuit block diagram showing the operation associated with Fig. 8;

 Figs. 10 to 12 are waveform diagrams showing the operation associated with Figs. 8 and 9;

20 Fig. 13 is a recording pattern diagram in a triple play mode using the head construction according to the present invention;

 Fig. 14 is a recording pattern diagram in a double play mode using the head construction according to
25 the present invention;

 Fig. 15 is a circuit block diagram showing an embodiment of the optimum tracking method at the time of reproduction in the sextuple play mode according to the

present invention;

Fig. 16 is a waveform diagram showing the operation of the circuit shown in Fig. 15;

Fig. 17 is a circuit diagram showing an embodiment of sextuple mode high-speed fast feed/rewind control means according to the present invention;

Fig. 18 is a pattern diagram showing the details of Fig. 13 in an enlarged form;

Fig. 19 is a pattern diagram showing the details of Fig. 7 in an enlarged form;

Fig. 20 is an image diagram showing an example of display of a video signal reproduced by the construction shown in Fig. 19;

Fig. 21 is a detailed relative positional relationship showing a relationship in tracking phase between a tape and heads at the time of reproduction of a pattern recorded in a quintuple play mode to which the present invention is applied;

Fig. 22 is a pattern diagram in an improved version of the pattern shown in Fig. 19;

Fig. 23 is a circuit diagram showing a detailed example of the circuit of Fig. 6 for realizing the relationship shown in Fig. 22;

Fig. 24 is a diagram showing a relative positional relationship representing a relationship in tracking phase between a tape and heads at the time of reproduction in a sextuple play mode according to another embodiment of the present invention; and

Fig. 25 is a circuit diagram showing an example of circuit means for realizing the relationship shown in Fig. 23.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

5 Embodiments of the present invention will now be described in detail on the basis of the accompanying drawings.

 First, a first embodiment of the present invention will be described using Figs. 1 to 4. Fig. 1
10 is a diagram showing the construction of heads on a drum according to the first embodiment. Fig. 2 is a diagram showing level differences between the heads in a head attachment height direction. Fig. 3 is a pattern diagram showing a relative positional relationship between a tape
15 and heads in a standard play recording mode. Fig. 4 is a pattern diagram showing a relative positional relationship between a tape and heads in a sextuple play mode.

 In Figs. 1 and 2, reference numeral 1 denotes a rotary drum, numerals 2 and 3 standard play video
20 recording/reproducing heads, numerals 4 and 5 sextuple play video recording/reproducing heads, and numerals 6 and 7 audio recording/reproducing heads.

 The pair of video heads 2 and 3 for standard play mode and the pair of video heads 4 and 6 for
25 sextuple play mode are arranged on the rotary drum 1 so that the paired heads have the interval of about 180 degree therebetween and their different azimuth angles.

Similarly, the pair of audio heads 6 and 7 are arranged so that they have the interval of about 180 degree therebetween and their different azimuth angles. The video heads 2 and 5 are arranged substantially in proximity to each other. The same holds for the video heads 3 and 4. An interval between those heads is set to be N times as long as a horizontal synchronizing signal period, wherein N is usually 1 or 2. The audio head 6 (or 7) and the video heads 3 and 4 (or 2 and 5) are arranged with an interval of 120 degree required therebetween. It is assumed that the rotating direction of the rotary drum 1 is anticlockwise, as is indicated by arrow. An example of an azimuth angle of each head formed between a gap plane of the head and a plane perpendicular to the rotating direction of the head is such that the video heads 2 and 4 have about +6 degree, the video heads 3 and 5 have about -6 degree, the audio head 6 has about +30 degree, and the audio head 7 has about -30 degree. Thereby, an azimuth loss is utilized to reduce a crosstalk between audio and video signals caused between adjacent tracks and in the same tracks.

The attaching levels or heights and the head widths of the video heads 2 to 5 and the audio heads 6 and 7 are as shown in Fig. 2.

Figs. 3 and 4 show recording track patterns when the recording is made on a magnetic tape by the head construction as mentioned above. In Figs. 3 and 4, the same portions or components as those in Figs. 1 and 2 are

denoted by the same reference numerals as those used in Figs. 1 and 2. Reference numeral 8 denotes a magnetic tape, numeral 9 an audio track, and numeral 10 a video track.

5 First, a relative positional relationship between the magnetic tape 8 and the heads 3 and 6 in a standard play recording mode is shown in Fig. 3. The tape speed is controlled so that each track pitch is about 60 μm . The head width of the audio head 6 is on
10 the order of about 28 μm with which an audio track 9 is formed on the magnetic tape 8. Delayed behind the audio head 6 by 120 degree on the rotary drum 1, the standard play video head 3 forms a video track 10 in such a manner that it is overwritten on the audio track 9. The delay
15 of 120 degree on the rotary drum 1 corresponds to the running of the magnetic tape equal to $(120 \text{ degree}) / (180 \text{ degree})$ of the track pitch (about 60 μm). In order that the overwriting is performed taking the tape running of 40 μm ($= 60 \mu\text{m} \times 120 / 180$) plus α into consideration, a
20 level difference between the heads 3 and 6 is selected to be about 58 μm . Plus α is a value for setting the audio track 9 so that it is substantially positioned at the vicinity of the center of the video track 10, as shown in Fig. 3. Thereby, the overlapping of different azimuth
25 polarity portions of the audio track 9 and the video track 10 spans about 28 μm . Also, it can be said that a proper head width for the video head 3 is about 60 μm which corresponds to the track pitch width. Generally,

an audio signal is recorded down to a deep layer portion of the magnetic tape 8 as a modulating signal with a relatively low frequency, and a video signal is recorded in a surface portion of the magnetic tape 8 as a
5 modulating signal with a relatively high frequency in a manner overwritten on the modulating signal of the audio signal while erasing of the same.

Next, a recording operation in a sextuple play mode will be described referring to Fig. 4 in connection
10 with a relative positional relationship between the magnetic tape 8 and the heads 4 and 6 in the sextuple play mode. The tape speed is controlled so that each track pitch is about 10 μm . The head width of the audio head 6 is on the order of about 28 μm with which an audio
15 track 9 is formed on the magnetic tape 8, as mentioned above. Delayed behind the audio head 6 by 120 degree on the rotary drum 1, the sextuple play video head 4 forms a video track 10 in such a manner that it is overwritten on the audio track 9. The delay of 120 degree on the rotary
20 drum 1 corresponds to the running of the magnetic tape equal to $(120 \text{ degree}) / (180 \text{ degree})$ of the track pitch (about 10 μm). Though there is a concept of selecting a level difference between the heads 4 and 6 to be about 7 μm with the tape running of about 7 μm ($= 10 \mu\text{m} \times$
25 $120/180$) being taken into consideration, the level difference selected in the shown example is about 49 μm for a reason which will be mentioned later on. Thereby, the overlapping of the same azimuth polarity portions of

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the audio track 9 and the video track 10 spans about 8 μm . However, since the azimuth angles of the video and audio heads 4 and 6 are different or 6 degree and 30 degree, respectively, as mentioned above, a sufficient azimuth loss is obtained so that an interference between video and audio signals is sufficiently removed. Also, it can be said that a proper head width for the video head 4 is about 20 μm which is sufficiently wide as compared with the track pitch width. This aims at the acquisition of a sufficient tracking performance even for the bend of the track or the like.

Next, a control of a recording completion point at the time of recording in such a sextuple play mode will be described in detail by use of Figs. 5 and 6. In Figs. 5 and 6, the same portions or components as those in Figs. 1 to 4 are denoted by the same reference numerals as those used in Figs. 1 to 4. Reference numeral 11 denotes an audio recording signal input terminal, numeral 12 an audio recording amplifier, numeral 13 a video recording signal input terminal, numeral 14 a video recording amplifier, and numeral 15 a timing control circuit for generation of mute signals to the recording amplifiers 12 and 14.

At the time of completion of recording, the audio recording/reproducing heads 6 and 7 precede. Therefore, if the supply of a recording signal to the audio recording/reproducing heads 6 and 7 and the supply of a recording signal to the video recording/reproducing

heads 4 and 5 are simultaneously stopped, there is left an area where only an audio signal is recorded. Accordingly, it is required to take a construction in which the supply of a recording signal to the video recording/reproducing heads 4 and 5 are continued by at least a time when the video recording/reproducing heads 4 and 5 certainly perform the overwriting on an audio track 9 recorded by the audio recording/reproducing heads 6 and 7. Namely, as shown in Fig. 6, an audio signal inputted from the audio recording signal input terminal 11 is supplied through the audio recording amplifier 12 to the audio recording/reproducing heads 6 and 7 while a video signal inputted from the video recording signal input terminal 13 is supplied through the video recording amplifier 14 to the video recording/reproducing heads 4 and 5, and the timings of stop of the supply of the recording signals from the audio and video recording amplifiers 12 and 14 to the heads 6 and 7 and the heads 4 and 5 are controlled by mute signals supplied from the timing control circuit 15. In Fig. 5, the mute signal to the video recording amplifier 14 is generated at a timing delayed from the supply of the mute signal to the audio recording amplifier 12 by $(5 + 120/180)$ tracks, that is, $(5 + 120/180)$ fields (or about 94.4 ms) so that the succeeding video recording/reproducing head 5 (and 4) can completely perform the overwriting for the preceding audio recording/reproducing head 6 (and 7).

Next, the arrangement of horizontal

synchronizing signals on the magnetic tape thus subjected to the recording is shown in Fig. 18 in conjunction with a triple play mode and in Fig. 19 in conjunction with a sextuple play mode with a VHS standard system being taken
5 as an example. According to the VHS standard, the deviation number (αH) of horizontal synchronizing signals (H) between adjacent tracks at the time of recording in the triple play mode is set to 0.5 H, as shown in Fig. 18. Therefore, when one field (262.5H) is recorded on
10 one track, the horizontal synchronizing signals (H) ensures an orderly H arrangement between adjacent recording tracks.

However, in the example of the sextuple play mode to which the present invention is applied, as shown
15 in Fig. 19, the deviation number αH is 0.25H so that the horizontal synchronizing signals (H) takes a disturbed H arrangement between recording tracks. When the magnetic tape subjected to such recording is subjected to reproduction by the head 4 which is wider in width than
20 the recording track shown in Fig. 19, the problem of leakage of signals from opposite adjacent tracks is liable to arise. In substance, though adjacent tracks are subjected to recording by heads having different azimuth angles so that an adjacent component is
25 reproduced with a level considerably lowered by virtue of an azimuth effect, for example, a horizontal synchronizing signal portion of relatively low frequency component in a low band converted chrominance signal or luminance

signal incapable of enjoying the azimuth effect especially leaks to give bad influence on the image quality. A monitored image at this time is shown in Fig. 20. Since horizontal synchronizing signal portions leaking from the opposite adjacent tracks deviate by $0.25H$ right and left respectively, as shown in Fig. 19, they appear as adjacent interfering signals in the form of two longitudinal stripes on the screen, as shown in Fig. 20, thereby deteriorating the image quality.

5 leaking from the opposite adjacent tracks deviate by
0.25H right and left respectively, as shown in Fig. 19,
they appear as adjacent interfering signals in the form
of two longitudinal stripes on the screen, as shown in
Fig. 20, thereby deteriorating the image quality.

10 An example of measures to counter the above-
mentioned effect from the opposite adjacent tracks is
shown in Fig. 21 in conjunction with a quintuple play
mode. With the recording in the quintuple play mode, the
effect from the opposite adjacent tracks is greatly
15 reduced as compared with that in the sextuple play mode.
Namely, the detection at the time of sextuple play mode
is the detection of 5 μm from opposite adjacent tracks
for 10 μm of a main track (ratio: $5/10 = 0.5$) whereas the
detection at the time of quintuple play mode is the
20 detection of 4 μm from opposite adjacent tracks for 12 μm
of a main track (ratio: $4/12 = 0.33$). The foregoing
description is made in connection with the example in
which the tracking control is performed so that the
detection is made equally from the right and left
25 adjacent tracks. In substance, however, it can be said
that to perform the reproduction while maintaining the
same positional relationship as that at the time of
recording enables the complete satisfaction of the same

condition as that at the time of recording and can cope with mechanical disturbing factors. Even in such a case, in the sextuple play mode, since the head end adjoins the same azimuth angle track which is the nearest but one adjacent track, there can be considered the nearest but one adjacent signal interference which results in the further deterioration of the image quality. From this point of view, too, the quintuple play mode is more effective. Further, it is needless to say that a plurality of longer play modes (for example, quintuple and sextuple play modes described in conjunction with the present embodiment) than the conventional triple play mode can be used in such a manner that they are switched, as required.

As a positive solving measure, Figs. 22 and 23 show an H arrangement realizing measure at the time of recording in the sextuple play mode. Fig. 23 shows an example of the specific circuit construction of the video recording amplifier 14 shown in Fig. 4. In Fig. 23, reference numerals 71 to 73 denote 0.25H delay circuits, numeral 74 a switching (SW) circuit, numeral 75 a recording amplifier, numeral 76 a switching (SW) circuit, and numeral 77 a delay control circuit. With this circuit construction, the H arrangement on each recording track can be ensured by switching the delay time in units of 0.25H for every recording track, as shown in Fig. 22. Namely, the H arrangement on all recording tracks can be realized by repeating four modes inclusive of $t_2 = 0.5H$,

$t_1 = 0.25H$, $t_0 = 0H$ and $t_3 = 0.75H$ for each recording track. Though the sextuple play mode has been described in conjunction with the present embodiment, it is needless to say that there is no limitation to such an example or the similar is possible for the quintuple play mode.

With the above construction, the positions of interfering signals from the nearest adjacent track and the nearest but one adjacent track assume the substantially same positions as horizontal synchronizing signals which do not appear on the monitor screen. The control for this purpose can be realized by supplying an output pattern of the above-mentioned four modes from the delay control circuit 77 of Fig. 23 in the video recording amplifier 14 to the SW circuit 74 in accordance with a signal from the timing control circuit 15 so that the optimum signal(s) is selected from the inputs/outputs of the $0.25H$ delay circuits 71 to 73 and is then supplied to the heads 4 and 5 through the recording amplifier 75 and the SW circuit 76. Thereby, the recording with the H arrangement as shown in Fig. 22 can be made on the magnetic tape.

Next, a reproducing operation in reproducing the signal thus recorded in the sextuple play mode will be described referring to Fig. 7 in connection with a relative positional relationship between the magnetic tape 8 and the heads 4 and 6. Though the basic relative relationship at the time of reproduction is similar to

that at the time of recording, the phases of the tape and the head are matched with each other, as shown in Fig. 7, in order to obtain the optimum tracking. Namely, the matching of tracking for the audio head 6 is made so that

5 a desired audio track 9 is substantially positioned at the center of the head 6. Thereby, the audio head makes the scanning on the nearest adjacent audio tracks on opposite sides but it does not make the scanning on the nearest but one adjacent tracks which have the same

10 azimuth as the desired track. Therefore, the head width of the audio head 6 (and 7) is set to be smaller than three times the track pitch width in the sextuple play mode (or audio head width $28\text{ }\mu\text{m} < \text{track pitch } 10\text{ }\mu\text{m} \times 3$). With this construction, it is possible to sufficiently

15 attenuate signals from the nearest adjacent tracks by virtue of azimuth loss and to prevent the nearest but one adjacent tracks from being subjected to reproduction, thereby enabling the reproduction of an audio signal for which a sufficient S/N is ensured. Since the audio head

20 6 is also used in a standard play mode, it is obvious that the possession of a head width as large as possible in the above-mentioned range is advantageous for the improvement in S/N ratio in the standard play mode.

Regarding the width of the video head 4 (and 5)

25 too, it is preferable that considering the reproduction of a tape subjected to recording by another magnetic recording/reproducing apparatus, the head width is set to be sufficiently large in a range smaller than three times

the track pitch width, in order that a track bend ($\pm 5 \mu\text{m}$) in the magnetic recording/reproducing apparatus in the present embodiment and the other magnetic recording/reproducing apparatus can sufficiently be absorbed. But, to make the head width larger than required results in the deterioration of S/N. Therefore, the proper width is $20 \mu\text{m}$ (track width $10 \mu\text{m}$ plus track bend $10 \mu\text{m}$) which is enough to cover the track bend and is about two times as large as the track pitch.

Next, the reason for setting the level difference of the video head 4 (and 5) relative to the audio head 6 (and 7) to about $49 \mu\text{m}$, as mentioned above, will be described using Figs. 8 and 9. Fig. 8 shows a reproducing operation in connection with a relative positional relationship between the magnetic tape 8 and the heads 3 and 4 when the magnetic tape 8 having been subjected to recording in a standard play mode is subjected to high-speed (in the reverse direction of the tape running direction at the time of recording and about three times as high as the recording speed) reproduction. Fig. 9 shows a circuit block diagram for obtaining the operation shown in Fig. 8. In Figs. 8 and 9, the same portions or components as those in Figs. 1 to 7 are denoted by the same reference numerals as those used in Figs. 1 to 7. Reference numerals 16 to 19 denote reproducing amplifiers, numerals 20 and 21 level comparators, and numerals 22 to 24 switching (SW) circuits. In high-speed reproduction, it is preferable that the video

heads 3 and 4 (or 2 and 5) provided adjacent to each other are arranged with different azimuth angles and a level difference between both the video heads is considered such that in the case where the output of the one video head 3 decreases, the output of the other video head 4 increases, as shown in Figs. 10 to 12. In the figures, reference numeral 25 denotes an output waveform indicating the output level of the video head 3 and numeral 26 denotes an output waveform indicating the output level of the video head 4. By selectively using the larger one of the outputs of both the video heads 3 and 4 (or switching the outputs of both the video heads 3 and 4 at equal intervals), there can be obtained a high-speed reproduction image in which the generation of noises is suppressed. For this purpose, it is preferable that the centers of the head widths of the video heads 3 and 4 are arranged substantially at the same level. The output waveforms 25 and 26 of the video heads 3 and 4 at this time are shown in Fig. 10. Also, considering the relative positional relationship at the time of recording in the sextuple play mode shown in Fig. 4, it is required that the sextuple play video head 4 (or 5) is arranged at a position with which it records succeeding (or delayed behind) the audio head 6 (or 7) by at least four fields (corresponding to four tracks) to six fields (corresponding to six tracks). This is obvious from Fig. 11 showing the output waveforms 25 and 26 of the video heads 3 and 4 at the time of high-speed reproduction in the case where

the recording is made succeeding by four fields and Fig. 12 showing the output waveforms 25 and 26 of the video heads 3 and 4 at the time of high-speed reproduction in the case where the recording is made succeeding by six
5 fields. Namely, it is seen that there can be obtained a high-speed reproduction image in which the generation of noises is suppressed. One circuit example for realizing the above is shown in Fig. 9. The outputs of the video recording/reproducing heads 3, 4, 5 and 2 are amplified
10 by the reproducing amplifiers 16, 17, 18 and 19, respectively. The level comparator 20 (or 21) inputted with the output signals of the reproducing amplifiers 16 and 17 (or 18 and 19) amplifying the outputs of the video recording/reproducing heads 3 and 4 (or 5 and 2) arranged
15 in proximity to each other detects the larger one of both the output signals. By selectively switching the switching circuit 22 (or 23) in accordance with the detected output signal, it is possible to select the larger output level always. The outputs of the switching circuits 22
20 and 23 are selectively switched in the switching circuit 24 by a head switching signal generated in synchronism with the rotation of the drum, thereby making it possible to obtain a continuous reproduction signal.

Instead of making the selection based on only
25 the magnitude of each reproducing amplifier output, the level comparator 20 or 21 can make the selection with which the respective periods (t_2 to t_3), (t_3 to t_4), (t_4 to t_5) and (sum of t_1 to t_2 and t_5 to t_6) become

equal, as shown in Figs. 10 to 12. In this case, there is a merit that an image changing point on the reproducing screen is fixed at the same point, thereby providing an image which is easy to see. Such selection can be realized by making a control so that the duty ratio of the output of the level comparator 20 or 21 takes 50 %.

Next, the operation at the time of recording/reproduction in a triple play mode will be described referring to Fig. 13 in connection with a relative positional relationship between the magnetic tape 8 and the heads 4 and 6. In Fig. 13, the same portions or components as those in Figs. 1 to 12 are denoted by the same reference numerals as those used in Figs. 1 to 12. The tape speed is controlled so that each track pitch is about 20 μm . The head width of the audio head 6 is on the order of about 28 μm with which an audio track 9 is formed on the magnetic tape 8, as mentioned above. Delayed behind the audio head 6 by 120 degree on the rotary drum 1, the sextuple play video head 4 forms a video track 10 in such a manner that it is overwritten on the audio track 9. Since the delay of 120 degree on the rotary drum 1 corresponds to the running of the magnetic tape equal to $(120 \text{ degree}) / (180 \text{ degree})$ of the track pitch (about 20 μm), the sextuple play video head 4 scans a position corresponding to a value (about 36 μm) obtained by subtracting the tape running of about 13 μm ($= 20 \mu\text{m} \times 120 / 180$) from the level difference (about 49 μm) between the heads 4 and 6. Thereby, the overlapping

of the same azimuth polarity portions of the audio track 9 and the video track 10 spans about $16\text{ }\mu\text{m}$. Also, the head width of the video head 4 is about $20\text{ }\mu\text{m}$ or ensures the track pitch width of about $20\text{ }\mu\text{m}$, it is possible to
5 perform the recording for all track pitches with a guard band being not generated. At the time of reproduction too, the reproduction can be performed with a substantially similar relation being kept.

Next, the operation at the time of recording/
10 reproduction in a double play mode will be described using Fig. 14 in connection with a relative positional relationship between the magnetic tape 8 and the heads 3 and 6. In Fig. 14, the same portions or components as those in Figs. 1 to 13 are denoted by the same reference
15 numerals as those used in Figs. 1 to 13. The tape speed is controlled so that each track pitch is about $30\text{ }\mu\text{m}$. The head width of the audio head 6 is on the order of about $28\text{ }\mu\text{m}$ with which an audio track 9 is formed on the magnetic tape 8, as mentioned above. Delayed behind the
20 audio head 6 by 120 degree on the rotary drum 1, the standard play video head 3 forms a video track 10 in such a manner that it is overwritten on the audio track 9. Since the delay of 120 degree on the rotary drum 1 corresponds to the running of the magnetic tape equal to
25 $(120\text{ degree})/(180\text{ degree})$ of the track pitch (about $30\text{ }\mu\text{m}$), the standard play video head 3 scans a position corresponding to a value (about $38\text{ }\mu\text{m}$) obtained by subtracting the tape running of about $20\text{ }\mu\text{m}$ ($= 30\text{ }\mu\text{m} \times$

120/180) from the level difference (about 58 μm) between the heads 3 and 6. Thereby, the overlapping of the same azimuth polarity portions of the audio track 9 and the video track 10 spans about 22 μm . Also, the head width of the audio head 6 is about 28 μm and hence a guard band of about 2 μm is generated for the track pitch width of about 30 μm . It is needless to say that at the time of reproduction too, the reproduction can be performed with a substantially similar relation being kept.

10 Thus, the recording or reproduction at the time of triple play mode can be realized by using the sextuple play video heads 4 and 5 and the recording or reproduction at the time of double play mode can be realized by using the standard play video heads 2 and 3.

15 Next, means for controlling the speed and phase of one of the tape and the head relative to the other in a magnetic recording/reproducing apparatus having various recording or reproducing modes with different tape speeds as mentioned above will now be described in detail while
20 the tracking for reproduction at the time of sextuple play mode shown in Fig. 7 is especially taken as an example. First, the construction for tracking will be described referring to Fig. 15. In Fig. 15, the same portions or components as those in Figs. 1 to 14 are
25 denoted by the same reference numerals as those used in Figs. 1 to 14. Reference numeral 27 denotes a drum motor for rotating the rotary drum 1, numeral 28 a capstan, numeral 29 a pinch roller, numeral 30 a capstan motor,

numeral 31 a head switching circuit for switching signals from the audio heads 6 and 7, numeral 32 a pre-amplifier for amplifying the output signal of the head, numeral 33 an audio signal processor circuit for performing a
5 demodulation and audio signal processing to restore a reproduction audio signal, numeral 34 an envelope detector circuit for detecting the amplitude component of an output signal of the pre-amplifier 32, numeral 35 a drum servo control circuit for controlling the speed and
10 phase of the drum motor 27 on the basis of a drum frequency generator (DFG) signal and a drum phase generator (DPG) signal which are generated by the drum motor 27, numeral 36 a head switching signal generator circuit for generating a timing for the switching of the
15 audio heads 6 and 7 on the basis of the DPG signal or the DFG signal normalized by the DPG signal, numerals 37 and 38 driver circuits for driving the motors, numeral 39 a capstan servo control circuit for controlling the tape running speed and phase on the basis of a CFG signal and
20 a control signal reproduced from the tape 8, numeral 40 a reference signal generator, numeral 41 a delay circuit, numeral 42 a tracking control circuit, numeral 43 a control head, numeral 44 an amplifier for reproducing a control signal, and numeral 45 a control system for the
25 drum and capstan of the magnetic recording/reproducing apparatus for controlling a relative positional relationship between the tape 8 and the audio heads 6 and 7.

In the above description of the construction,

portions for performing electrical processings are all represented as circuits. However, a portion enclosed by dotted line 45 may be replaced by a proper microcomputer or may be constructed by software. Numeral 86 indicates
5 a mode switching circuit between the tape speed and the drum rotating speed

Next, the operation of the present embodiment will be described using Fig. 16 together with Fig. 15. A signal on a helically scanned audio track 9 recorded on
10 the tape 8 is reproduced by the two audio heads 6 and 7 arranged on the rotary drum 1. The outputs of the audio heads 6 and 7 are alternately selected and read by the switching circuit 31. The signal is amplified by the pre-amplifier 32 and is then supplied to the audio signal
15 processor circuit 33 and the envelope detector circuit 34. The audio signal processor circuit 33 outputs an audio signal subjected to a demodulation processing. Though not shown, the similar is made for a video signal. Namely, the video signal is reproduced by the standard
20 play video heads 2 and 3 or the sextuple play video heads 4 and 5 arranged on the rotary drum 1. Then, a continuous reproduction signal is obtained through a switching circuit and is thereafter subjected to a demodulation processing to output a demodulation
25 processed video signal.

On the other hand, the drum servo processing or control circuit 35 generates a control signal to keep the period of a DFG signal constant and also compares the

phases of a DPG signal and an output signal of the reference signal generator 40 to perform the phase synchronization of both the signals with each other. Thereby, the speed and phase of the drum motor 27 are controlled.

Also, the capstan servo processing or control circuit 39 generates a speed control signal to keep the period of a capstan frequency generator (CFG) signal constant and also compares the phase of a control signal obtained through the control head 43 and the reproducing amplifier 44 from the tape 8 and a signal obtained through the delay circuit 41 from the reference signal generator 40 to perform the phase synchronization of both the signals with each other.

A tracking control using the capstan motor 30 is created as follows. First, the envelope detector circuit 34 detects the amplitude component of a signal read from the tape 8. An output signal of the envelope detector circuit 34 takes, for example, such a form as shown in Fig. 16, by virtue of a relative relationship between the audio track 9 formed on the tape 8 and the trace phase of the audio head 6 or 7. Namely, since the width of the audio track 9 is about 10 μm whereas the width of the audio head 6 or 7 is about 28 μm , the outputs from the nearest adjacent tracks are not substantially subjected to reproduction owing to the azimuth effect but the outputs from the nearest but one adjacent tracks are subjected to reproduction owing to

the same azimuth. Therefore, when the audio head 6 or 7 traces the center of the reverse azimuth track, reproduction output levels corresponding to 9 μ m are respectively detected from the same azimuth adjacent tracks on

5 opposite sides of the reverse azimuth track (see the positional relationship of the audio head 6 indicated by dotted line in Fig. 16). However, since the same azimuth adjacent tracks have no correlation therebetween, they include signal components cancelled from each other so

10 that the signal level of each track is lowered as compared with a signal level reproduced from the same track. Thus, a relative output level has a change, as shown in a lower portion of Fig. 16, for a change in phase of one of the audio track 9 and the audio head 6 or

15 7 to the other thereof. Using these results, the optimum tracking phase is set using the delay circuit 41. The optimum value can be obtained, for example, by detecting phase positions at which output levels on opposite sides become equal to each other, as shown in Fig. 16 and

20 setting the optimum tracking phase to a center value between the detected phase positions.

Next, another embodiment of the present invention will be described referring to Figs. 24 and 25. In the present embodiment, the description will be made

25 of a method in which a long play recording is performed lowering not only the tape feed speed mentioned until now but also the rotating speed of the rotary head. Fig. 24 is a diagram showing a relative position relationship

between a recording track on a magnetic tape and recording heads at the time of recording in the sextuple play mode in the present invention. Fig. 25 shows detailed specific circuit means in the drum servo processing or control circuit 35 shown in Fig. 15, for making the detailed description of specific circuit means which realizes the relationship shown in Fig. 24. In Fig. 25, reference numeral 78 denotes a $\times 2$ multiplier circuit, numerals 79 and 80 switching (SW) circuits, numeral 81 a speed detector circuit, numeral 82 a phase detector circuit, numeral 83 an adder circuit, numeral 84 an input terminal for an instruction designating the sextuple play mode in the present invention, and numeral 85 a $1/2$ demultiplier circuit.

A recording pattern shown in Fig. 24 is the same as the recording pattern in the triple play mode shown in Fig. 13. However, a recorded signal is different. Namely, in the conventional triple play mode shown in Fig. 13, one track is recorded with a video signal corresponding to one field. On the other hand, in the present embodiment, one track is recorded with a video signal corresponding to two fields so that a double amount of information is recorded. This system is realized by setting the running speed of the magnetic tape to the sextuple play mode while setting the rotating speed of the rotary head to $1/2$. With this construction, it is possible to generate a recording track pattern free of interfering signals from the nearest adjacent tracks

and the nearest but one adjacent tracks at the time of reproduction mentioned above. Of course, since the relative speed between the magnetic tape and the rotary head is lowered, it is required that attention should be

5 directed to the deterioration of the high frequency component of a frequency modulated video signal. However, a sufficient performance is obtained if the recording/reproduction in a normal mode is made using the recent magnetic tape and head which can realize a high

10 resolution mode (corresponding to an S-VHS mode in the case of the VHS system). Therefore, it is preferable that the recording mode in the present embodiment is limited to, for example, a mode which can be set only in the case where the S-VHS cassette tape is inserted.

15 Next, specific means for realizing the present method will be described in detail by use of Figs. 15 and 25. Since the control of the magnetic tape in the sextuple mode has already been described by use of Fig. 15, specific circuit means for controlling the speed of

20 the rotary head into 1/2 will now be described by use of Fig. 25. Fig. 25 shows a circuit construction provided in the drum servo control circuit 35 which controls the rotation of the rotary head. In the present long play (or sextuple play) mode contrasted with a normal mode,

25 the switching circuits 79 and 80 operates in accordance with an instruction from the input terminal 84 so that a DFG signal generated by the rotating speed of the drum having the rotary head is supplied to the x2 multiplier

circuit 78 so that a double frequency is provided. The double frequency is supplied through the switching circuit 79 to the speed detector circuit 81 and further to the adder circuit 83 to control the drum motor. As a
5 result, therefore, the rotary head is controlled at a speed which is $1/2$ as compared with that in the normal mode. As to the phase detector circuit 82, a signal from the reference signal generator circuit 40 is subjected to $1/2$ frequency division by the $1/2$ demultiplier circuit 85
10 and is then supplied through the switching circuit 80 to the phase detector circuit 82 which is also inputted with a drum rotation phase signal DPG. Thus, the $1/2$ speed control can be performed similarly for the phase control too.

15 Also, it is easy to realize a construction in which though not shown, the type of a magnetic tape being inserted at present is detected by a system controller so that a signal inputted to the input terminal 84 can set the above-mentioned long play recording mode, for
20 example, only in the case where an S-VHS tape is used.

Though the recording of two fields on one track has been described in conjunction with the present embodiment. However, as can easily be understood, it is possible to construct a system in which three or more
25 fields are recorded on one track.

Next, a high-speed fast feed/rewind operation for a magnetic tape 8 in the present invention will be described in detail by use of a block diagram shown in

Fig. 17. In Fig. 17, the same portions or components as those in Figs. 1 to 16 are denoted by the same reference numerals those used in Figs. 1 to 16. In Fig. 17, reference numerals 46 and 47 denote reel, numerals 48 and 5 49 reel stands, numeral 50 a generator for generating FG (Frequency Generator) pulses obtained in proportion to the rotating speed of the reel stand 48, numeral 51 a generator for generating FG pulses obtained in proportion to the rotating speed of the reel stand 49, numerals 52 10 and 53 brakes, numeral 54 a motor, numeral 55 a driving power transmission unit for transmitting a rotational driving power of the motor 54 to the reel stand 48 or 49, numeral 56 a generator for generating FG pulses obtained in proportion to the rotating speed of the motor 54, 15 numeral 57 a winding radius detector, numeral 58 a speed detector, numeral 59 a deceleration setting unit or deceleration controller, numeral 60 a target or reference speed switching unit, numeral 61 a speed error detector, numeral 62 a PWM generator or pulse width modulator, 20 numeral 63 an integrator, numeral 64 a motor driver, numeral 65 a brake controller, numeral 66 a brake mechanism driver, numeral 67 a data detector, numeral 68 an adder, and numerals 69 and 70 input terminals.

Though the rotary drum 1 and the capstan 28 are 25 not shown in Fig. 17, they are provided adjoining the magnetic tape 8 transferred between the reels 46 and 47. The following description referring to Fig. 17 will be made in conjunction with the fast feed/rewind operation

in which the magnetic tape 8 is transferred between the reels 46 and 47 at a high speed. First, the description will be made of the operation in the case where the magnetic tape 8 runs at a speed of V_n .

- 5 The motor 54 is rotationally driven by an output signal from the motor driver 64. A driving power of the motor 54 is transmitted through the driving power transmission unit 55 to the reel stand 49 at the time of fast feed and the reel stand 48 at the time of rewind.
- 10 Thereby, the magnetic tape 8 is wound on the reel 47 at the time of fast feed and the reel 46 at the time of rewind. At this time, the speeds of the reel stand 48, the reel stand 49 and the motor 54 are detected by the FG oscillators 50, 51 and 56, respectively. Frequencies
- 15 indicating the detected rotating speeds of the reel stands 48 and 49 and the motor 54 are inputted to the winding radius detector 57 and the speed detector 58.

- The winding detector 57 detects the winding radius R_s or R_t of the reel 46 or 47, for example, in
- 20 accordance with the following equation (1):

$$\begin{aligned} R_s &= (S/(\pi(1 + (T_t/T_s)^2)))^{1/2} \\ R_t &= (S/(\pi(1 + (T_s/T_t)^2)))^{1/2} \end{aligned} \quad \dots (1)$$

- wherein S is the total winding area of the tape inclusive of the reel hub when the tape is seen from above, and T_s
- 25 and T_t are the periods of frequencies obtained from the FG oscillators 50 and 51.

 Also, the speed detector 58 detects the running speed V of the tape, for example, in accordance with the

following equation (2):

$$V = 2\pi \cdot R_t / T_t. \quad \dots (2)$$

The radius R_s or R_t detected by the winding radius detector 57 is inputted to the speed detector 58 and the deceleration controller 59. Also, the speed data V detected by the speed detector 58 is inputted to the speed error detector 61 and the brake controller 65.

In the deceleration controller 59, a deceleration \underline{d} causing no tape looseness at the time of deceleration is set on the basis of the winding radius value R_s or R_t inputted from the winding radius detector 57. In order to perform a deceleration run having no tape looseness, it is required that the deceleration \underline{d} of the tape winding reel subjected to control should be set to a value not larger than a deceleration caused by a load torque of the tape supplying reel subjected to no control. Namely, the deceleration \underline{d} [mm/s^2] is set in accordance with the following equation (3):

$$a \leq T \cdot R / I \quad \dots (3)$$

wherein T , R and I are the load torque [gr/mm], winding radius [mm] and moment of inertia [gr/mm^2] of the tape supplying reel, respectively. It is necessary that the load torque T and the moment of inertia I are determined beforehand by measurement or the like. The tape supplying reel is the reel 46 at the time of fast feed and the reel 47 at the time of rewind.

The deceleration \underline{d} set by the deceleration controller 59 is inputted to the reference speed

switching unit 60. In the reference speed switching unit 60, a reference or target speed V_n is set by a speed switching signal inputted through the input terminal 70. The set reference speed V_n is inputted to the speed error
5 detector 61. The speed error detector 61 determines an error component between the speed data V detected by the speed detector 58 and the reference speed V_n set by the reference speed switching means 60. The speed error component determined by the speed error detector 61 is
10 fed back to the motor 54 through the PWM generator 62, the integrator 63 and the motor driver 64 so that the tape running speed V follows the reference speed V_n .

At the time of such high-speed fast feed/
rewind, there is an operation in which an index signal or
15 VISS (VHS Index Search System) signal recorded, for example, on a control signal by means of duty ratio modulation is detected from the magnetic tape 8 to stop the running of the magnetic tape 8. In Fig. 17, the index signal superimposed on the control signal on the
20 magnetic tape 8 is detected by the data detector 67 through the control head 43. An output of the data detector 67 is inputted to the reference speed switching unit 60 and the brake controller 65 through the adder 68. The reference speed switching unit 60 inputted with this
25 stop operating signal starts the subtraction from the reference speed V_n . The amount of subtraction for the reference speed V_n per unit time is proportional to the deceleration \underline{a} inputted from the deceleration controller

59. Thereby, the reference speed V_n changes with a gradient corresponding to the deceleration \underline{d} . Since the running speed V follows the reference speed V_n , the running speed V is decelerated at the deceleration \underline{d} . On the other hand, the brake controller 65 inputted with the stop operating signal judges whether or not the speed data V inputted from the speed detector 58 becomes smaller than an allowable speed V_L and outputs a brake acceptance signal when V becomes smaller than V_L . The brake acceptance signal outputted from the brake controller 65 is inputted to the brake mechanism driver 66. The brake mechanism driver 66 drives the brakes 52 and 53 in accordance with the brake acceptance signal from the brake controller 65 to stop the running of the tape.

Accordingly, if the reference speed V_n outputted from the reference speed switching unit 60 is a speed V_H which is above the allowable speed V_L , a brake acceptance signal is outputted from the brake controller 65 after the deceleration from the speed V_H to the speed V_L subsequent to the input of a stop operating signal, thereby stopping the running. Since the deceleration changes as the winding radius of the supplying reel changes, the timing of brake is different for each winding radius.

Also, if the reference speed V_n is lower than the allowable speed V_L , a stop operation is such that the brake controller 65 outputs a brake acceptance signal

simultaneously with the input of a stop operating signal to stop the running.

By using a construction in which the output of the reference speed switching unit 60 is switched in accordance with which one of modes from the standard play mode to the sextuple play mode the magnetic tape 8 is recorded in, the convenience of use by purposes can be improved. Namely, in the case of designating a mode in which the magnetic tape 8 is to be merely rewound up to its head portion, the setting to the most fast rewinding speed suffices irrespective of the recording mode. However, at the time of fast feed/rewind in a mode in which the running of the tape is stopped in accordance with the detection of an index signal superimposed on a control signal, as mentioned above, the frequency of a control signal reproduced from a magnetic tape 8 is such that even at the same tape speed, a frequency detected from a magnetic tape subjected to recording in a sextuple play mode is six times as high as that detected from a magnetic subjected to recording in a standard play mode. In this case, there may be considered a possibility that the frequency of a reproduction control signal becomes too high for the control signal to be detected. The reproduction control signal is used as information for managing a tape position by virtue of the number of signals. Therefore, if the detection of the reproduction control signal is not possible, there results in a defective system. Also, even if the number of reproduction

control signals can be detected, the system is defective if an index signal superimposed on the reproduction control signal cannot be detected. For such circumstances, means for limiting a high-speed fast feed/rewind

- 5 speed at the time of sextuple mode is provided. This high-speed fast feed or rewind speed is set by supplying a speed switching signal to the reference speed switching unit 60 from the input terminal 70. Thereby, even for a tape subjected to recording in the newly provided
- 10 sextuple play mode, it is possible to realize, even in the high-speed fast feed/rewind mode, a search control in which an index signal superimposed on a control signal on the tape is detected to stop the tape at a desired position.

- 15 Also, the judgement of a recording mode at the time of reproduction can be made through the comparison of a normally reproduced control signal frequency and the speed of a magnetic tape.

- The input terminal 69 is provided for inputting
- 20 a stop operating signal when an operator performs a stop operation manually.

The motor 54 in the foregoing description may be the same as the capstan motor 30 shown in Fig. 15.

- In a recording/reproducing apparatus and a
- 25 reproducing apparatus according to the present invention as mentioned above, the recording/reproduction of an audio signal in both a standard play mode and a long play mode or N-ple play mode (N: an integer not smaller than

4) can be realized by a common audio head in regard to the recording or reproduction of a video signal and an audio signal. Also, an N-ple play mode video head can be used in common for realizing the recording/reproduction
5 of a video signal in a triple play mode. Further, a standard play mode video head can be used in common for realizing the recording/reproduction of a video signal in a double play mode.

With a construction in which an audio head
10 output is used as a tracking method at the time of reproduction in the N-ple play mode, it is possible to perform the optimum tracking for both audio and video. Also, with a construction in which at the time of completion of recording in the N-ple play mode, a video
15 signal is supplied with a time prolonged corresponding to the delay of scan of a video head from that of an audio head, it is possible to surely overwrite a video track on an audio track. Further, with a construction in which a high-speed fast feed/rewind speed at the time of N-ple
20 play mode is set to a low value as compared with the tape speed at the time of standard play mode, the detection of an index signal from the tape in the N-ple play mode can be ensured.

While we have shown and described several
25 embodiments in accordance with our invention, it should be understood that disclosed embodiments are susceptible of changes and modifications without departing from scope of the invention. Therefore, we do not intend to be

bound by the details shown and described herein but intend to cover all such changes and modifications falling within the ambit of the appended claims.

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